

METHOD FOR MEASURING ELECTROMAGNETIC RADIATION PATTERN AND
GAIN OF RADIATOR USING TEM WAVEGUIDE

Technical Field

5 The present invention relates to a method for measuring an electromagnetic radiation pattern and gain of a radiator; and, more particularly, to a method for measuring the electromagnetic radiation pattern and gain of a radiator by electrically modeling the radiator based on powers of output
10 ports of a traverse electric and magnetic (TEM) waveguide wherein the powers are measured for eighteen (18) arrangements of the radiator after locating the radiator within the TEM waveguide.

Background Art

15 Figs. 1 and 2 are diagrams illustrating a conventional radiation power measurement method wherein an electromagnetic signal is directly received from an antenna in an open area test site (OATS) or an anechoic chamber.

20 As shown, a maximum radiation power or an effective radiation power (ERP) is measured in a standard test site, e.g., an open area test sites (OATS) or an anechoic chamber. The conventional radiation power measurement method will be described.

25 An equipment under test (EUT) 101 is located on a turntable of the standard test site (step 1), a transmission antenna 102 is located to be opposite to a test antenna 103, and then a signal having the highest power is written by moving the test antenna up and down ranging a few meters, e.g., in case of ANSI std., 1 m ~ 6 m (step 2). By rotating the turntable 100 by a predetermined
30 angle, e.g., ANSI std., 45 °, seven additional values are written by repeating the step 2 (Step 3). Then, the transmitter under test 101 is replaced with a half-wave vertical antenna 112 (step 4). The half-wave vertical antenna 112 should be located so that the center of the antenna is identical to that of the EUT, and
35 the antenna is connected to a radio frequency (RF) signal

generator 111 having known output values. Path losses are written and an effective radiation power (ERP) is computed based on the path losses.

5 The conventional radiation power measurement method is based on an ElectroMagnetic Interference (EMI) measurement method, and measures/estimates the maximum radiation power or the ERP by receiving an electromagnetic signal on the antenna in the OATS or anechoic chamber.

10 However, the conventional radiation power measurement method performed in the OATS or the anechoic chamber have drawbacks that it takes much time to measure radiation from a test object because of direct measurement by antenna, a maintenance fee for the standard test site costs high, and there are a lot of measurement errors because of environmental 15 uncertainty.

Also, in estimation of the ERP/a total radiation power (TRP), it is preferred that a radiation field is estimated on spherical surface in free space. However, the conventional measuring method uses a cylindrical scanning method, and therefore, there is a 20 drawback that a receiving field can be devaluated.

Fig. 3 is a diagram showing a conventional radiation power measurement method in a semi-anechoic chamber, and Fig. 4 is a diagram showing a conventional radiation power measurement method in an anechoic chamber.

25 Referring to Fig. 3, the conventional radiation power measurement method in the semi-anechoic chamber has the same drawbacks as the conventional radiation power measurement method described above with reference to Figs. 1 and 2. The conventional measuring method takes a long time to measure the power and a 30 high maintenance fee. Also, since there is reflection due to the ground plane, a measurement error is large. The conventional measuring method uses a sphere scan, and the radiation field can be devaluated. In the conventional measuring method in the anechoic chamber described with reference to Fig. 4, the 35 measurement error is small, however, it take a long time to measure

the power and a high maintenance fee.

Summary of the Invention

It is, therefore, an object of the present invention to
5 provide a method for measuring the electromagnetic radiation
pattern and gain of a radiator by electrically modeling the
radiator based on powers of output ports of a traverse electric
and magnetic (TEM) waveguide wherein the powers are measured
for eighteen (18) arrangements of the radiator after locating
10 the radiator within the TEM waveguide.

In accordance with an aspect of the present invention, there
is provided a method for measuring a radiation pattern and a
gain of a radiator, including the steps of: a) measuring powers
of output port of a transverse electric and magnetic (TEM)
15 waveguide by changing arrangements of the radiator located within
the TEM waveguide; and b) estimating a radiation power density
of the radiator in free space, wherein the radiator is modeled
as a dipole moment based on the powers of the output port of
the TEM waveguide.

20 The method as recited in claim 1, further includes the steps
of: c) measuring a power P_0 received by an antenna of the radiator
based on a conducted power accepted by the radiator and a
reflecting coefficient of an antenna of the radiator, and
obtaining a maximum radiation power density P_D of a half-wave
25 dipole antenna due to the power P_0 at a predetermined distance;
d) obtaining the maximum radiation power density P_{max} among the
estimated radiation power densities; e) obtaining a radiation
gain of the radiator based on the maximum radiation power density
 P_{max} obtained in the step d) and the maximum radiation power density
30 P_D obtained in the step d); and f) obtaining an effective radiation
power based on the maximum radiation power density P_{max} , wherein
the maximum radiation power density P_D of a half-wave dipole
antenna due to the power P_0 at a predetermined distance is obtained
by an equation as:

$$P_D = \frac{P_o \cdot (\text{gain of half - wave dipole antenna measured in TEM waveguide})}{4\pi R^2}$$

Brief Description of the Drawings

5 The above and other objects and features of the present invention will become apparent from the following description of the preferred embodiments given in conjunction with the accompanying drawings, in which:

10 Figs. 1 and 2 are diagrams illustrating a conventional radiation power measurement method wherein an electromagnetic signal is directly received from an antenna in an open area test site (OATS) or an anechoic chamber;

15 Fig. 3 is a diagram showing a conventional radiation power measurement method in a semi-anechoic chamber;

20 Fig. 4 is a diagram showing a conventional radiation power measurement method in an anechoic chamber;

25 Fig. 5 is a diagram illustrating a radiation pattern and gain measurement system using TEM waveguide to which the present invention is applied;

30 Fig. 6 is a diagram depicting modeling electronic/magnetic dipole of EUT to which the present invention is applied;

35 Figs. 7 and 8 are diagrams depicting coordinate system of the TEM waveguide and the EUT to which the present invention is applied;

40 Figs. 9 and 10 are flow charts illustrating a method for measuring a radiation pattern and gain of a radiator based on TEM waveguide in accordance with the present invention;

45 Fig. 11 is a diagram illustrating a cell height in the TEM waveguide;

50 Fig. 12 is a flow chart illustrating a method for measuring powers $P_1 \sim P_{18}$ of the output port of the TEM waveguide for eighteen (18) arrangements of EUT in accordance with the present invention; and

55 Figs. 12 to 18 are diagrams illustrating a method for

measuring powers $P_1 \sim P_{18}$ of the output port of the TEM waveguide for eighteen (18) arrangements of EUT in accordance with the present invention.

5 Best Mode for Carrying Out the Invention

Other objects and aspects of the invention will become apparent from the following description of the embodiments with reference to the accompanying drawings, which is set forth
10 hereinafter.

Fig. 5 is a diagram illustrating a radiation pattern and gain measurement system using TEM waveguide to which the present invention is applied.

In order to overcome problem of the conventional measuring
15 method, for the EMI measurement, there are many tries that the measurement on the ground is replaced with measurement in transverse electric and magnetic (TEM) waveguide. Some of the measurements in TEM waveguide are standardized by international special committee on radio interference (CISPR).

20 The TEM waveguide means a device transferring the TEM mode, e.g., TEM cell, Gigahertz Transverse ElectroMagnetic cell (GTEM cell), and has at least one port.

25 In the present invention, since it is used a power of one port of the TEM waveguide, and a various kinds of TEM waveguides can be used.

As shown, the TEM waveguide has a rectangular shape enlarged
30 from a coaxial cable so that characteristic impedance is kept. The TEM waveguide is a device transferring a TEM mode, the EUT is located within the TEM waveguide, a power of an output port of the TEM waveguide is measured and electromagnetic modeling of the EUT is performed based on the output power.

The EUT is an electromagnetic element to be measured for a radiation field, for an accurate measurement, the size of the EUT is proper to be within uniform field of the TEM waveguide.

35 For accurate modeling of the EUT within the TEM waveguide,

the EUT should be located in various directions, such that the EUT is electromagnetically modeled based on the power of output port of the TEM waveguide for each direction.

In general, the EUT is assumed to be a pair of an electronic dipole moment and a magnetic dipole moment. A phase difference between the moments, of which vectors are orthogonal to each other, is considered or disregarded according to a modeling algorithm. In other words, the number of arrangements and rotation angles of the EUT in the TEM waveguide are decided according to the modeling algorithm.

Hereinafter, a system for measuring a radiation pattern and gain of the EUT in the TEM waveguide will be described with reference to Fig. 5.

As shown, the radiation pattern and gain measurement system includes TEM waveguide 40, a EUT 41, a coaxial cable 42, a power receiver 43 and a personal computer unit 44.

The EUT 41 is located in the TEM waveguide, and the output port of the TEM waveguide is connected to the coaxial cable 42. The EUT is a radiator which can be modeled as an equivalent dipole, because the EUT is an electronically small.

The TEM waveguide is a measurement system having an outer conductor which electromagnetically shields from the outside and has a shielding window so as to monitor the EUT in the outside, and an inner conductor which is a septum. When the EUT 41 is operated in normal condition after locating the EUT 41 in the TEM waveguide 40, power radiating from the EUT 41 is received the power receiver 43 through the output port of the TEM waveguide.

The coaxial cable 42 is connected to the output port of the TEM waveguide and the power receiver 43, and the power receiver 43 measures the power radiated from the EUT 41 through the coaxial cable 42.

The power receiver 43 informs the personal computer unit 44 of the measured power levels. The personal computer unit 44 estimates a radiation pattern of the EUT 41 modeled as the equivalent dipole in a free space based on the measured power.

Estimation of electromagnetic interference (EMI) using the TEM waveguide is performed by calculating the maximum radiation value from an EUT with the waveguide output powers and reporting the value as an EMI result. The maximum radiation value is obtained by simulating the radiation field under assumption that the modeled EUT is located on the ground plane such as the OATS or semi-anechoic chamber.

A common feature in the measurements of the EMI and the ERP is to find the maximum electric field in a standard test field. The measurement of the EMI is terminated by compensating the maximum power regarding losses in the receiving antenna and the cable. The measurement of the ERP performs additional steps of obtaining a gain relative to a half-wave dipole antenna and multiplying the power transmitted to the antenna of the EUT by the gain.

Fig. 6 is a diagram depicting modeling electronic/magnetic dipole of EUT to which the present invention is applied.

In the present invention, a small radiator (EUT) 500 is located in the TEM waveguide, the power of the output port of the TEM waveguide is measured by changing the arrangement of the EUT eighteen times, and the gain and the radiation pattern of the EUT are measured by electromagnetically modeling the EUT based on the eighteen power values.

As shown, the EUT is modeled as an electric dipole having three elements orthogonal to each other and a magnetic dipole having three elements orthogonal to each other. In order for accurate modeling, it is considered relative phase difference among x, y and z elements of the dipole moment.

The detection of the maximum radiation, which includes measurement of the radiation field in the test chamber, e.g., the anechoic chamber, is performed by assuming a radiation field from the modeled electronic dipole and the magnetic dipole.

Figs. 7 and 8 are diagrams depicting coordinate system of the TEM waveguide and the EUT to which the present invention is applied.

As shown, a reference coordinate system of the TEM waveguide is X, Y, Z (Fig. 7), and a reference coordinate system of the EUT is X', Y', Z' (Fig. 8), which are in general.

The power of the output ports of the TEM waveguide is related
5 to the reference coordinate system of the TEM waveguide (Fig. 7), and the radiation pattern of the radiator is related to the reference coordinate system of the EUT is X', Y', Z' (Fig. 8).

Figs. 9 and 10 are flow charts illustrating a method for measuring a radiation pattern and gain of a radiator based on
10 TEM waveguide in accordance with the present invention.

In this embodiment, a gain, an ERP and a TRP of the radiator are measured in the TEM waveguide without a receiving antenna.

At step S701, a conducted power P_M transmitted to the EUT and a reflection coefficient M_2 of the antenna of the EUT are
15 measured.

At step S702, a power P_0 accepted by the antenna of the EUT is obtained based on the conducted power P_M and the reflection coefficient M_2 by an equation 1 as:

20
$$P_0 = P_M \times (1 - M_2) \quad \text{Eq. (1)}$$

At step S703, the maximum radiated power density (P_D) of a half-wave dipole to the equal power P_0 within a measuring distance R is calculated by an equation 2 as:
25

$$P_D = \frac{P_0 \cdot 1.64}{4\pi R^2} \quad \text{Eq. (2)}$$

In Eq. (2), it is preferred to use a gain of the half-wavelength dipole, which is measured in the TEM waveguide
30 in real, instead of the absolute gain, 1.64, of the half-wavelength dipole.

At step S704, a distance between the septum and the outer conductor is measured at a position of the EUT, the distance is referred to as "H" (See Fig. 11). Since an intensity of the

electromagnetic field formed in the cell is changed based on H, H is necessary for normalizing the power of the output port of the TEM waveguide.

At step S706, powers P₁ to P₁₈ of the output port of the TEM waveguide are measured and stored. Herein, P₁ to P₁₈ are obtained by locating the EUT on a height H in the TEM waveguide. The frequency of the measured power is the same frequency as a target frequency of the ERP or TRP to be measured. The frequency can be a single frequency or a frequency having a bandwidth.

The powers of the output ports of the TEM waveguide is normalized by dividing the powers by $\left(\frac{1}{2}e_{0y}\right)^2$ when 1.0 W is applied to the TEM waveguide, which is expressed in Equation 3 as:

$$P_n = \frac{P_n}{\left(\frac{1}{2}e_{0y}\right)^2} \quad \text{Eq. (3)}$$

$$e_{0y} = \frac{1}{H} \sqrt{P_{unit} \cdot Z_0} = \frac{1}{H} \sqrt{50}$$

wherein, e_{0y} is a fundamental mode, i.e., an orthogonal element in an electrical field of the TEM mode when a unit power is applied to the TEM waveguide.

Step 705 including steps 706 and 707 is a procedure of measuring powers of the output ports of the TEM waveguide related to estimate the radiation field by measuring the EUT.

At step 708, the radiation power of the EUT in the free space is estimated based on the powers P₁ to P₁₈ by using a following Equation 6.

In order to estimate radiation power, the radiation field is scanned. Representative scan method includes a cylindrical scan and a spherical scan. Hereinafter, the sphere scan is described.

A radiation power density P(r, Θ, ϕ) of the EUT on a sphere having a radius r in free space is obtained based on the powers

P₁ to P₁₈ of the output port of the TEM waveguide and an equation (6).

First, at step 709 and 710, let the radius of the sphere be R=r, and Θ be 0 [rad], at steps 712 to 714, the radiation power density P(r, Θ, φ) of the EUT on a virtual sphere in free space is measured by changing φ from 0 to 2π [rad]. The radiation power density P(r, Θ, φ) is obtained by the powers P₁ to P₁₈ of the output port of the TEM waveguide into the Equation (6) and the spherical coordinate system. The radiation power density P(r, Θ, φ) represents a radiation power density P(r, Θ, φ) on a position in spherical coordinate system.

In other words, at step 714, Θ and φ are set by 0 [rad], the radiation power density is obtained, and then the radiation power density on (r, 0, Δφ) in spherical coordinate system. These procedures are repeated until φ=2π [rad].

At step 715, Θ is increased by ΔΘ, at steps 712 to 714, the radiation power density is obtained by changing φ from 0 to 2π [rad]. These procedures are repeated until φ=π [rad] at steps 711 to 716.

In other words, the sphere scan is procedures of obtaining a radiation power density P(r, Θ, φ) of the EUT on a sphere having a radius r in free space based on the powers P₁ to P₁₈ of the output port of the TEM waveguide and an equation (6).

The equation (6) is obtained based on following equations (4) and (5). In the cylinder scan or scanning for a certain area, if a position on which the radiation power density is to be obtained is converted to the sphere coordinate system, the equation (6) can be directly applied.

$$P(\theta, \phi) = \frac{1}{2} R_e ((E \times H^\phi) \cdot \hat{a}_r) \quad \text{Eq. (4)}$$

$$= \frac{1}{2} R_e ((E_\theta \hat{a}_\theta + E_\phi \hat{a}_\phi) \times (H_\theta \hat{a}_\theta + H_\phi \hat{a}_\phi)^\ast) \cdot \hat{a}_r$$

$$\begin{aligned}
&= \frac{1}{2} R_e \left(H_\phi H_\phi^\phi \eta_0 + H_\theta H_\theta^\theta \eta_0 \right) \cdot \hat{a}_r \cdot \hat{a}_r \\
&= \frac{\eta}{2} R_e \left\{ \left[-\frac{j k_0 e^{-j k_0 r}}{4\pi r} \left(N_\theta + \frac{L_\phi}{\eta_0} \right) \right] \left[-\frac{j k_0 e^{-j k_0 r}}{4\pi r} \left(N_\theta + \frac{L_\phi}{\eta_0} \right) \right]^\phi \right. \\
&\quad \left. + \left[\frac{j k_0 e^{-j k_0 r}}{4\pi r} \left(N_\phi - \frac{L_\theta}{\eta_0} \right) \right] \left[\frac{j k_0 e^{-j k_0 r}}{4\pi r} \left(N_\phi - \frac{L_\theta}{\eta_0} \right) \right]^\phi \right\}
\end{aligned}$$

where

$$\begin{aligned}
N_\theta &= \iint_s (P'_x \cos \theta \cos \phi + P'_y \cos \theta \sin \phi - P'_z \sin \theta) e^{+jk' r' \cos \varphi} ds' \\
N_\phi &= \iint_s (-P'_x \sin \phi + P'_y \cos \phi) e^{+jk' r' \cos \varphi} ds' \\
L_\theta &= \iint_s (M'_x \cos \theta \cos \phi + M'_y \cos \theta \sin \phi - M'_z \sin \theta) e^{+jk_0 r' \cos \varphi} ds' \\
L_\phi &= \iint_s (-M'_x \sin \phi + M'_y \cos \phi) e^{+jk_0 r' \cos \varphi} ds'
\end{aligned}$$

10

$$P(\theta, \phi) = \frac{15\pi}{r^2 \lambda^2} \left\{ \begin{aligned}
&\left[P_x'^2 + k_0^2 M_x'^2 \right] \cos^2 \theta \cos^2 \phi + \sin^2 \phi \left[P_y'^2 + k_0^2 M_y'^2 \right] \cos^2 \theta \sin^2 \phi + \cos^2 \phi \left[P_z'^2 + k_0^2 M_z'^2 \right] \sin^2 \theta \\
&- 2 \left[P_x' P_y' \cos(\varphi_{px} - \varphi_{py}) + k_0^2 M_x' M_y' \cos(\varphi_{mx} - \varphi_{my}) \right] \sin^2 \theta \sin \phi \cos \phi \\
&- 2 \left[P_y' P_z' \cos(\varphi_{py} - \varphi_{pz}) + k_0^2 M_y' M_z' \cos(\varphi_{my} - \varphi_{mz}) \right] \sin \theta \cos \theta \sin \phi \\
&- 2 \left[P_z' P_x' \cos(\varphi_{pz} - \varphi_{px}) + k_0^2 M_z' M_x' \cos(\varphi_{mz} - \varphi_{mx}) \right] \sin \theta \cos \theta \cos \phi \\
&+ 2k_0 \left[P_x' M_y' \sin(\varphi_{px} - \varphi_{my}) - P_y' M_x' \sin(\varphi_{py} - \varphi_{mx}) \right] \cos \theta \\
&+ 2k_0 \left[P_y' M_z' \sin(\varphi_{py} - \varphi_{mz}) - P_{yx}' M_y' \sin(\varphi_{pz} - \varphi_{my}) \right] \sin \theta \cos \phi \\
&+ 2k_0 \left[P_z' M_x' \sin(\varphi_{pz} - \varphi_{mx}) - P_x' M_z' \sin(\varphi_{px} - \varphi_{mz}) \right] \sin \theta \sin \phi
\end{aligned} \right\}$$

Eq. (5)

$$P(\theta, \phi) = \frac{15\pi}{r^2 \lambda^2} \left\{ \begin{aligned}
&\left[A + k_0^2 D \right] \cos^2 \theta \cos^2 \phi + \sin^2 \phi \left[B + k_0^2 B \right] \cos^2 \theta \sin^2 \phi + \cos^2 \phi \left[C + k_0^2 F \right] \sin^2 \theta \\
&- 2 \left[G + k_0^2 J \right] \sin^2 \theta \sin \phi \cos \phi - 2 \left[H + k_0^2 K \right] \sin \theta \cos \theta \sin \phi - 2 \left[I + k_0^2 L \right] \sin \theta \cos \theta \cos \phi \\
&+ 2k_0 [M - P] \cos \theta + 2k_0 [N - Q] \sin \theta \cos \phi + 2k_0 [O - R] \sin \theta \sin \phi
\end{aligned} \right\}$$

15

Eq. (6)

where

$$A + k_0^2 D = \frac{1}{4} (P_1 + P_4 + P_{11} + P_{14} - P_3 - P_5 + P_8 + P_{10} + P_{13} + P_{15} - P_6 - P_9)$$

$$B + k_0^2 B = \frac{1}{4} (P_1 + P_4 + P_6 + P_9 - P_8 - P_{10} + P_3 + P_5 + P_{13} + P_{15} - P_{11} - P_{14})$$

$$C + k_0^2 F = \frac{1}{4} (P_6 + P_9 + P_{11} + P_{14} - P_{13} - P_{15} + P_3 + P_5 + P_8 + P_{10} - P_1 - P_4)$$

$$5 \quad G = P_{18} - \frac{(P_3 + P_5 + P_{11} + P_{14}) + \sqrt{2}(P_3 - P_5 + P_{11} - P_{14})}{4}$$

$$J = \frac{4P_7 - (P_6 + P_8 + P_9 + P_{10}) + \sqrt{2}(P_9 - P_6 + P_{10} - P_8)}{4k_0^2}$$

$$H = P_{16} - \frac{(P_1 + P_4 + P_8 + P_{10}) + \sqrt{2}(P_1 - P_4 + P_8 - P_{10})}{4}$$

$$K = \frac{4P_{12} - (P_{11} + P_{13} + P_{14} + P_{15}) + \sqrt{2}(P_{14} - P_{11} + P_{15} - P_{18})}{4k_0^2}$$

$$I = P_{17} - \frac{(P_6 + P_9 + P_{13} + P_{15}) + \sqrt{2}(P_6 - P_9 + P_{13} - P_{15})}{4}$$

$$10 \quad L = \frac{4P_2 - (P_1 + P_3 + P_4 + P_5) + \sqrt{2}(P_4 - P_1 + P_5 - P_8)}{4k_0^2}$$

$$M = \frac{P_{15} - P_{13}}{4k_0^2} \quad P = \frac{P_4 - P_1}{4k_0^2} \quad N = \frac{P_5 - P_3}{4k_0^2}$$

$$Q = \frac{P_9 - P_6}{4k_0^2} \quad O = \frac{P_{10} - P_8}{4k_0^2} \quad R = \frac{P_{14} - P_{11}}{4k_0^2}$$

15 Eq. (5) represents a radiation power density on a spherical coordinates (r, θ, ϕ) to the electric dipole moment P and the magnetic dipole moment M . Since the dipole moments P and M can be expressed by an equation related to the power of the output port of the TEM waveguide, and the radiation power density in a desired scan area can be obtained by putting the powers P_1 to P_{18} of the output port of the TEM waveguide to the equation (6).

At step 717, it is obtained the maximum power density $P_{\max}(r, \theta_0, \phi_0)$ among the radiation power densities obtained at the steps

709 to 716.

Next, at step 718, a relative gain, a total radiation power (TRP) and an effective radiation power (ERP) are calculated based on following equations (7) and (8).

5

$$\text{relative gain } g = \frac{P_{\max}}{P_D} \quad \text{Eq. (7)}$$

$$\text{relative gain } G[dBd] = 10 \log \left(\frac{P_{\max}}{P_D} \right)$$

$$TRP = \int_0^{360^\circ} \int_0^{180^\circ} P(r, \theta, \phi) r^2 \sin \theta d\theta d\phi \quad \text{Eq. (8)}$$

10

Eq. (8) represents sphere integration to an electric density on a spherical having a radius r .

$$ERP = \frac{P_{\max} \cdot 4\pi R^2}{1.64} \quad \text{Eq. (9)}$$

15

In the equation (9), it is preferred that an absolute gain of the half-wave dipole antenna, 1.64, is replaced with a gain of the half-wave dipole antenna, wherein the gain is measured 20 with the TEM waveguide.

Fig. 11 is a diagram illustrating a cell height in the TEM waveguide.

As shown, a distance between the septum 81 and the outer conductor is measured at a position of the EUT within the TEM 25 waveguide, and the distance is referred to as a cell height H . According to the cell height H , an intensity of the electric field is varied.

In order to obtain more accurate powers of the output port of the TEM waveguide, the maximum length of a side of the EUT 30 should be shorter than $H/3$ of the TEM waveguide.

Figs. 9 and 10 are flow charts illustrating a method for

measuring powers $P_1 \sim P_{18}$ of the output port of the TEM waveguide for eighteen (18) direction of EUT in accordance with the present invention.

It is simply described the method for measuring powers $P_1 \sim P_{18}$ of the output port of the TEM waveguide for eighteen (18) arrangements of EUT with reference to Fig.9. Detailed method for measuring powers $P_1 \sim P_{18}$ of the output port of the TEM waveguide is illustrated with reference to Fig. 11.

After locating the EUT within the TEM waveguide at step 900, a reference coordinate system (X , Y , Z) of the TEM waveguide is putted to a reference coordinate system (X , Y , Z) of the EUT, and the powers $P_1 \sim P_{18}$ of the output port of the TEM waveguide for eighteen (18) arrangements of the EUT are measured by rotating the EUT on X-axe or Y-axe at steps 901 to 912.

At step 901, in case of a coordinate system (XX' , YY' , ZZ'), the powers P_1 to P_5 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 0° , 45° , 90° , 180° and 270° on Y-axis. Wherein the position (XX' , YY' , ZZ') means the EUT coordinate axes X' , Y' and Z' are putted to GTEM coordinate axes X , Y , Z , respectively.

At step 904, in case of a coordinate system (XY' , YZ' , ZX'), the powers P_6 to P_{10} of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 0° , 45° , 90° , 180° and 270° on Y-axis. Wherein the position (XY' , YZ' , ZX') means the EUT coordinate axes X' , Y' and Z' are putted to GTEM coordinate axes Y , Z , X , respectively.

At step 906, in case of a coordinate system (XZ' , YX' , ZY'), the powers P_{11} to P_{15} of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 0° , 45° , 90° , 180° and 270° on Y-axis. Wherein the position (XZ' , YX' , ZY') means the EUT coordinate axes X' , Y' and Z' are putted to GTEM coordinate axes Z , X , Y , respectively.

At steps 907 and 908, in case of a coordinate system (XX' , YY' , ZZ'), the power P_{16} of the output port of the TEM waveguide

is measured after rotating the EUT counterclockwise by 45° on X-axis.

At steps 909 and 910, in case of a coordinate system (XY', YZ', ZX'), the power P_{17} of the output port of the TEM waveguide 5 is measured after rotating the EUT counterclockwise by 45° on X-axis.

At steps 911 and 912, in case of a coordinate system (XZ', YX', ZY'), the powers P_{11} to P_{15} of the output port of the TEM waveguide 10 is measured after rotating the EUT counterclockwise by 45° on X-axis.

Figs. 12 to 17 are diagrams illustrating a method for measuring powers P_1 ~ P_{18} of the output port of the TEM waveguide for eighteen (18) arrangements of EUT in accordance with the present invention.

15 In general, after putting the reference coordinate system of the EUT to the reference coordinate system of the TEM waveguide, the measurement of the powers for eighteen arrangements of the EUT is performed. However, orders in the measurement of the powers for eighteen arrangements of the EUT can be changed.

20 After putting the reference coordinate system (X', Y', Z') of the EUT to the reference coordinate system (X, Y, Z) of the TEM waveguide, the powers for arrangements 1 to 5 of the EUT are measured by rotating the EUT counterclockwise on Y-axis. (Fig. 13)

25 Arrangement 1: In case of a coordinate system (XX', YY', ZZ'), a power P_1 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 0° (i.e., no rotation) on Y-axis. Wherein the position (XX', YY', ZZ') means the EUT coordinate axes X', Y' and Z' are putted to GTEM coordinate 30 axes X, Y, Z, respectively.

Arrangement 2: In case of the coordinate system (XX', YY', ZZ'), a power P_2 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 45° on Y-axis.

Arrangement 3: In case of the coordinate system (XX', YY',

$ZZ')$, a power P_3 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 90° on Y-axis.

Arrangement 4: In case of the coordinate system (XX' , YY' , $ZZ')$, a power P_4 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 180° on Y-axis.

Arrangement 5: In case of the coordinate system (XX' , YY' , $ZZ')$, a power P_5 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 270° on Y-axis.

After measuring powers for the five arrangements of the EUT, powers P_6 to P_{11} for next five arrangements of the EUT are measured. After putting the reference coordinate system (Y' , Z' , $X')$ of the EUT to the reference coordinate system (X , Y , Z) of the TEM waveguide, the powers for arrangements 6 to 10 of the EUT are measured by rotating the EUT counterclockwise on Y-axis. (Fig. 14)

Arrangement 6: In case of the coordinate system (XY' , YZ' , $ZX')$, a power P_6 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 0° (i.e., no rotation) on Y-axis. Wherein the position (XX' , YY' , $ZZ')$ means the EUT coordinate axes X' , Y' and Z' are putted to GTEM coordinate axes Y , Z , X , respectively.

Arrangement 7: In case of the coordinate system (XY' , YZ' , $ZX')$, a power P_7 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 45° on Y-axis.

Arrangement 8: In case of the coordinate system (XY' , YZ' , $ZX')$, a power P_8 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 90° on Y-axis.

Arrangement 9: In case of the coordinate system (XY' , YZ' , $ZX')$, a power P_9 of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 180° on Y-axis.

Arrangement 10: In case of the coordinate system (XY' , YZ' , $ZX')$, a power P_{10} of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 270° on Y-axis.

After putting the reference coordinate system (Z' , X' , $Y')$

of the EUT to the reference coordinate system (X, Y, Z) of the TEM waveguide, the powers for arrangements 11 to 15 of the EUT are measured by rotating the EUT counterclockwise on Y-axis. (Fig. 15)

5 Arrangement 11: In case of the coordinate system (XZ',
YX', ZY'), a power P_{11} of the output port of the TEM waveguide
is measured after rotating the EUT counterclockwise by 0° (i.e.,
no rotation) on Y-axis. Wherein the position (XX', YY', ZZ')
means the EUT coordinate axes X', Y' and Z' are putted to GTEM
10 coordinate axes Y, Z, X, respectively.

Arrangement 12: In case of the coordinate system (XZ', YX',
ZY'), a power P_{12} of the output port of the TEM waveguide is measured
after rotating the EUT counterclockwise by 45° on Y-axis.

15 Arrangement 13: In case of the coordinate system (XZ',
YX', ZY'), a power P_{13} of the output port of the TEM waveguide
is measured after rotating the EUT counterclockwise by 90° on
Y-axis.

20 Arrangement 14: In case of the coordinate system (XZ',
YX', ZY'), a power P_{14} of the output port of the TEM waveguide
is measured after rotating the EUT counterclockwise by 180°
on Y-axis.

25 Arrangement 15: In case of the coordinate system (XZ',
YX', ZY'), a power P_{15} of the output port of the TEM waveguide
is measured after rotating the EUT counterclockwise by 270°
on Y-axis.

Arrangements 16 to 18 are implemented by rotating the EUT
on X-axis, which will be hereinafter.

30 Arrangement 16: In case of the coordinate system (XX',
YY', ZZ'), a power P_{16} of the output port of the TEM waveguide
is measured after rotating the EUT counterclockwise by 45° on
X-axis. (Fig. 16)

Arrangement 17: In case of the coordinate system (XY', YZ',
ZX'), a power P_{17} of the output port of the TEM waveguide is measured
after rotating the EUT counterclockwise by 45° on X-axis. (Fig.

17)

Arrangement 18: In case of the coordinate system (XZ' , YX' , ZY'), a power P_{18} of the output port of the TEM waveguide is measured after rotating the EUT counterclockwise by 45° on X-axis. (Fig. 5 18)

The measured powers P_1 to P_{18} of output ports of the TEM waveguide are used to estimate radiation power in free space. (Figs. 9 and 10)

When estimating radiation performance of the transmitter, 10 the conventional measuring method requires a test site, e.g., the OATS or the anechoic chamber, the receiver, the receiving antenna, the antenna master, a controller for mechanically moving the antenna. However, the measuring method in accordance with the present invention has less measurement error and reduces 15 time and cost to measure the power.

By changing arrangements of the EUT within the TEM waveguide, the powers of the output port of the TEM waveguide are measured, and radiation patterns of the EUT can be obtained based on the minimum arrangements rapidly and accurately.

20 While the present invention has been described with respect to certain preferred embodiments, it will be apparent to those skilled in the art that various changes and modifications may be made without departing from the scope of the invention as defined in the following claims.